

Particle Filtering for Attitude Estimation Using a Minimal Local-Error Representation

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I. Introduction

Spacecraft attitude estimation is the process of determining the orientation of the spacecraft with respect to a reference frame. Many nonlinear filtering methods have been applied to spacecraft attitude estimation. The extended Kalman filter (EKF) has been the most widely used nonlinear filtering method for realtime attitude estimation so far [1]. It works well in the linear regime where the linear approximation of the nonlinear dynamical system and observation model is valid. An unscented Kalman filter (UKF) has been proposed for attitude estimation, which uses a set of deterministically chosen *sigma points* to more accurately map a probability distribution and which is more robust than the EKF under large initial attitude-error conditions [2]. Other improved nonlinear filtering algorithms for attitude estimation are surveyed in [3]. Most of these algorithms estimate the mean and covariance of the state vector based on second- or higher-order approximations of nonlinear functions. Although the mean and covariance are the sufficient statistics of a Gaussian distribution, they are not sufficient to represent a general probability distribution. When these methods are applied to strongly nonlinear and non-Gaussian estimation problems, where the probability distribution of the state vector may be multi-modal, heavy-tailed, or skewed, desired performance characteristics may not be obtained.

Particle filters (PFs) [4] have gained much attention in recent years. Like other approximate nonlinear filtering methods, the ultimate objective of the PF is to reconstruct

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the posterior probability density function (pdf) of the state vector, or the probability distribution of the state vector conditional on all the available measurements. However, the approximation of the PF is vastly different from that of conventional nonlinear filters. By approximating a continuous distribution of interest by a finite (but large) number of weighted random samples or particles in the state space, the PF assumes no functional form for the posterior probability distribution. In the simplest form of the PF, the particles are propagated through the dynamic model and then weighted according to the likelihood function, which determines how closely the particles match the measurements. Those that best match the measurements are multiplied and those that do not are discarded. In principle, the PF (with an infinity of particles) can approximate the posterior probability distribution of any form and solve any nonlinear and/or non-Gaussian estimation problem. In practice, however, it is nontrivial to design a PF with a relatively small number of particles. The performance of the PF heavily depends on whether the particles are located in the significant regions of the state space and whether the significant regions are covered by the particles. When the measurements are accurate, which is typical for spacecraft attitude estimation and many other estimation problems, the likelihood function concentrates in a small region of the state space and the particles propagated through the dynamic model are more often than not located outside the significant regions of the likelihood function. State estimates such as the mean and covariance approximated with these particles are imprecise. This problem with the PF becomes even worse when the initial estimation errors are large, for example, a few orders of magnitude larger than the sensor accuracy. In this paper a PF based on the idea of progressive correction [5] is given, which maintains diversity of the particles and guides the particles to the right regions of the state space gradually, thus improving the computational efficiency of the filter.

A quaternion-based PF for spacecraft attitude estimation has been introduced in [6]. The quaternion representation is preferred over other representations because of the bilinear nature of the kinematics, which has a closed-form discrete-time solution, and because it contains no singularities [7]. However the unity norm of the quaternion must be maintained. If the quaternion estimate is given by a weighted sum of quaternion particles, then it is not guaranteed to preserve the norm constraint. A normalized quaternion estimate can be obtained based on either the minimum mean-square error [6,8] or maximum *a posteriori* [6] approach. Neither approach requires brute-force quaternion normalization. In this paper the problem due to the quaternion constraint is circumvented by using an unconstrained representation for the local error-space. The approach is similar to the concept in the UKF of [2] but differences exist that will be seen here. The covariance of the attitude error and the gyro bias used in progressive correction is computed based on the local error-representation as well. Note that the multiplicative quaternion errors may also be used in progressive correc-

tion and the associated attitude error covariance may be computed from the multiplicative quaternion errors using the method of [9]. The proposed PF estimates the attitude and gyro bias simultaneously. By contrast, the filter of [6] is a genetic-algorithm-embedded quaternion particle filter that estimates the attitude quaternion using a particle filter and the gyro bias using a genetic algorithm. The PF of [10] estimates both the attitude and the attitude rate in a gyro-less scenario, but employs different efficiency improving strategies.

The organization of this paper proceeds as follows. First, the PF is reviewed. Then, a brief review of the quaternion attitude kinematics and gyro model is provided. Next, an attitude estimation PF using a local-error representation is provided. Finally, the PF is compared with the EKF and UKF using simulated three-axis magnetometer (TAM) and gyro measurements of an Earth-pointing spacecraft.

II. Particle Filtering

The particular PF proposed for attitude estimation is based on the Bootstrap Filter (BF) or the Sampling Importance Resampling algorithm (with regularization) [11], which is reviewed in this section. A general discrete-time state-space model consists of the system dynamical model and the measurement model. The system model relates the current state vector, \mathbf{x}_k , to the one-stage ahead state vector, \mathbf{x}_{k+1} , and the measurement model relates the state vector \mathbf{x}_k to the measurement vector $\tilde{\mathbf{y}}_k$:

$$\mathbf{x}_{k+1} = \mathbf{f}_k(\mathbf{x}_k, \mathbf{u}_k, \mathbf{w}_k) \quad (1a)$$

$$\tilde{\mathbf{y}}_k = \mathbf{h}_k(\mathbf{x}_k, \mathbf{v}_k) \quad (1b)$$

In the above equations the system and measurement functions are denoted by \mathbf{f}_k and \mathbf{h}_k , respectively. The subscript k in \mathbf{f}_k and \mathbf{h}_k indicates that the functions themselves can be time-varying. The measurement sampling period is denoted by $\Delta t = t_{k+1} - t_k$. The vector \mathbf{u}_k is the deterministic input. The process noise \mathbf{w}_k and the measurement noise \mathbf{v}_k are assumed to be zero-mean white noise sequences. The distributions of the mutually independent \mathbf{x}_0 , \mathbf{w}_k , and \mathbf{v}_k , denoted by $p_{\mathbf{x}_0}(\mathbf{x}_0)$, $p_{\mathbf{w}_k}(\mathbf{w}_k)$ and $p_{\mathbf{v}_k}(\mathbf{v}_k)$, respectively, are assumed to be known. No Gaussian assumptions for these distributions are needed.

Now the procedure of a BF with N weighted particles is reviewed. The sets of particles and their associated weights at t_k and t_{k+1} are denoted by $\{\mathbf{x}_k^{(i)}, w_k^{(i)}\}$ and $\{\mathbf{x}_{k+1}^{(i)}, w_{k+1}^{(i)}\}$, respectively, where $i = 1, \dots, N$. Four steps, namely, prediction, update (correction), resampling and regularization (roughening), constitute a filter cycle.

At the prediction step, the particles are propagated through the following equation while their weights remain unchanged: $\mathbf{x}_{k+1}^{(i)} = \mathbf{f}_k(\mathbf{x}_k^{(i)}, \mathbf{u}_k, \mathbf{w}_k^{(i)})$, where N samples $\mathbf{w}_k^{(i)}$ of the

process noise are drawn according to the pdf $p_{\mathbf{w}_k}(\mathbf{w}_k)$, denoted by $\mathbf{w}_k^{(i)} \sim p_{\mathbf{w}_k}(\mathbf{w}_k)$, $i = 1, \dots, N$. At the update step that follows, the weight associated with each particle is updated based on the likelihood function $p_{k+1}(\tilde{\mathbf{y}}_{k+1} | \mathbf{x}_{k+1}^{(i)})$:

$$\tilde{w}_{k+1}^{(i)} = w_k^{(i)} p(\tilde{\mathbf{y}}_{k+1} | \mathbf{x}_{k+1}^{(i)}) \quad (2a)$$

$$w_{k+1}^{(i)} = \frac{\tilde{w}_{k+1}^{(i)}}{\sum_{i=1}^N \tilde{w}_{k+1}^{(i)}} \quad (2b)$$

where $\tilde{w}_{k+1}^{(i)}$ denotes the unnormalized weight. Note that $\sum_{i=1}^N w_{k+1}^{(i)} = 1$ after normalization is done by Eq. (2b). When the measurement noise is additive, $\tilde{\mathbf{y}}_{k+1} = \mathbf{h}_{k+1}(\mathbf{x}_{k+1}) + \mathbf{v}_{k+1}$, the likelihood function has a simple form: $p_{k+1}(\tilde{\mathbf{y}}_{k+1} | \mathbf{x}_{k+1}^{(i)}) = p_{\mathbf{v}_{k+1}}(\tilde{\mathbf{y}}_{k+1} - \mathbf{h}_k(\mathbf{x}_{k+1}^{(i)}))$.

The prediction and update steps implement a cycle of the sequential importance sampling algorithm. The variance associated with the weights in sequential importance sampling can only increase over time and eventually all but one particle will have negligible weight [12]. A common practice to overcome this degeneracy problem is resampling. The resampling scheme discards particles with small weights and multiplies particles with large weights. It is implemented by drawing samples (with replacement) N times from $\{\mathbf{x}_{k+1}^{(i)}, w_{k+1}^{(i)}\}$ to obtain N equally weighted particles, $\{\mathbf{x}_{k+1}^{(i)}, 1/N\}$. The total number of particles remains unchanged and no new particles are created by resampling. The normalized weight $w_{k+1}^{(i)}$ may be interpreted as the probability of occurrence for each particle. The probability of the particle $\mathbf{x}_{k+1}^{(i)}$ being chosen once in the resampling process is approximately $w_{k+1}^{(i)}$ and after resampling $\mathbf{x}_{k+1}^{(i)}$ will be multiplied approximately $(Nw_{k+1}^{(i)})$ times. The resampling algorithm is a black-box algorithm that takes as input the normalized weights and particle indices, and outputs new indices. It has nothing to do with the particles' dimension, values, and so on.

Since resampling may generate many identical particles and therefore greatly decreases the number of distinct particles, it is usually followed by a regularization step, which adds small noise to the resampled particles to increase particle diversity [5]: $\mathbf{x}_{k+1}^{(i)} \leftarrow \mathbf{x}_{k+1}^{(i)} + \boldsymbol{\nu}_{k+1}^{(i)}$, with \leftarrow denoting *assigned to* and $\boldsymbol{\nu}_{k+1}^{(i)}$ a small independent jitter drawn from a Gaussian distribution $\mathcal{N}(\mathbf{0}, h^2 \Sigma_{k+1})$, where h^2 is a tuning parameter and

$$\Sigma_{k+1} = \frac{1}{N-1} \sum_{i=1}^N \tilde{\mathbf{x}}_{k+1}^{(i)} \tilde{\mathbf{x}}_{k+1}^{(i)T} \quad (3a)$$

$$\tilde{\mathbf{x}}_{k+1}^{(i)} = \mathbf{x}_{k+1}^{(i)} - \hat{\mathbf{x}}_{k+1} \quad (3b)$$

$$\hat{\mathbf{x}}_{k+1} = \frac{1}{N} \sum_{i=1}^N \mathbf{x}_{k+1}^{(i)} \quad (3c)$$

Note that Σ is not a function of the particle weights. In tuning h , tradeoffs have to be

made between spawning more distinct particles (large noise) and not altering the original distribution too much (small noise). The optimal choice for h for the Gaussian kernel is [5]

$$h_{\text{opt}} = \left(\frac{4}{N(n_x + 2)} \right)^{\frac{1}{n_x + 4}} \quad (4)$$

where n_x is the dimension of the state vector.

The resampling and regularization steps are used to guarantee the proper performance of the BF, but are not required for processing the filter. They may be applied at every cycle, as in the original BF, or when the effective sample size, N_{eff} , is small. If resampling is done at every cycle, then all weights at the end of the cycle are identical and Eq. (2a) reduces to $w_{k+1}^{(i)} = p(\tilde{\mathbf{Y}}_{k+1} | \mathbf{x}_{k+1}^{(i)})$. The effective sample size is approximated by $N_{\text{eff}} \approx 1 / \sum_{i=1}^N (w_{k+1}^{(i)})^2$, which is a measure of the variation of the (normalized) weights [4]. If only very few particles have significant weights while others are negligible (the sum is always 1), then $N_{\text{eff}} \approx 1$; if all the particles are nearly equally weighted, then $N_{\text{eff}} \approx N$. Usually, large N_{eff} is desired, but large N_{eff} alone does not necessarily mean vast diversity among particles, because N_{eff} is not a function of the particles $\mathbf{x}_{k+1}^{(i)}$ and large N_{eff} may correspond to the unfavorable case in which most of the particles are identical (due to resampling). The side effect of resampling and regularization is that they introduce additional Monte Carlo variations. The resampling step has the ‘‘cut-tail’’ effect and results in many identical particles. Applying resampling too frequently may eliminate potentially good particles as well. The regularization step increases the sample covariance of the particles.

In the BF as well as other PFs, what is the most essential in the evolution of the filter is the particles and their associated weights. The estimates such as the mean and covariance are derived from the particles and computed using the following equations:

$$\hat{\mathbf{x}}_{k+1}^+ = E\{\mathbf{x}_{k+1} | \tilde{\mathbf{Y}}_{k+1}\} \approx \sum_{i=1}^N w_{k+1}^{(i)} \mathbf{x}_{k+1}^{(i)} \quad (5a)$$

$$P_{k+1} = E\{(\mathbf{x}_{k+1} - \hat{\mathbf{x}}_{k+1}^+)(\mathbf{x}_{k+1} - \hat{\mathbf{x}}_{k+1}^+)^T | \tilde{\mathbf{Y}}_{k+1}\} \approx \sum_{i=1}^N w_{k+1}^{(i)} \tilde{\mathbf{x}}_{k+1}^{(i)} \tilde{\mathbf{x}}_{k+1}^{(i)T} \quad (5b)$$

where $\tilde{\mathbf{x}}_{k+1}^{(i)} = \mathbf{x}_{k+1}^{(i)} - \hat{\mathbf{x}}_{k+1}^+$ and $\tilde{\mathbf{Y}}_{k+1}$ denotes the set of measurements up to and including t_{k+1} . The superscript + is used to denote updated value because a distinction between propagated and updated values is needed in the attitude estimation PF. It is advised that when the mean and covariance are computed, they should be computed after the update but before resampling and regularization [4].

The BF makes few assumptions about the dynamical system and measurement models, and involves only straightforward function evaluations and random sampling schemes, thus

it is very easy to implement. The function evaluations include the system function, measurement function, and the likelihood function (possibly up to a constant). The following sampling steps are needed: draw samples from $p_{\mathbf{x}_0}(\mathbf{x}_0)$ at the initial time, draw samples from $p_{\mathbf{w}_k}(\mathbf{w}_k)$ at the prediction step, generate uniform random numbers at the resampling step, and draw samples from $\mathcal{N}(\mathbf{0}, h^2 \Sigma_{k+1})$ at the regularization step. Note that in the BF it is not required to draw samples from the likelihood or evaluate the prior.

III. Attitude Kinematics and Sensor Models

The attitude matrix A is a proper orthogonal matrix, i.e. its inverse is given by its transpose and its determinant is +1. For spacecraft applications the attitude mapping is usually applied from the reference frame to the spacecraft body frame. Mathematically, the mapping from the reference frame to the body frame is given by $\mathbf{b} = A\mathbf{r}$, where \mathbf{b} is the body-frame representation of a vector and \mathbf{r} is the reference-frame representation of the vector. The quaternion used to represent the attitude is defined as a four-dimensional unit vector, given by $\mathbf{q} \equiv [\boldsymbol{\rho}^T \ q_4]^T$, with $\boldsymbol{\rho} \equiv [q_1 \ q_2 \ q_3]^T = \mathbf{e} \sin(\vartheta/2)$ and $q_4 = \cos(\vartheta/2)$, where \mathbf{e} is the unit Euler axis and ϑ is the rotation angle. The elements of $\boldsymbol{\rho}$ correspond to the purely imaginary part of the quaternion as proposed by Hamilton: $q_4 + q_1\mathbf{i} + q_2\mathbf{j} + q_3\mathbf{k}$, with \mathbf{i} , \mathbf{j} , and \mathbf{k} the imaginary units. Since a four-dimensional vector is used to describe three dimensions, the quaternion components cannot be independent of each other. The quaternion satisfies a single constraint given by $\mathbf{q}^T \mathbf{q} = 1$. The attitude matrix is related to the quaternion by $A(\mathbf{q}) = (q_4^2 - \|\boldsymbol{\rho}\|^2) I_{3 \times 3} + 2\boldsymbol{\rho} \boldsymbol{\rho}^T - 2q_4[\boldsymbol{\rho} \times]$, where $I_{3 \times 3}$ is a 3×3 identity matrix and $[\boldsymbol{\rho} \times]$ is the standard cross product matrix defined by [3]

$$[\boldsymbol{\rho} \times] \equiv \begin{bmatrix} 0 & -q_3 & q_2 \\ q_3 & 0 & -q_1 \\ -q_2 & q_1 & 0 \end{bmatrix} \quad (6)$$

The quaternion kinematics equation is given by

$$\dot{\mathbf{q}} = \begin{bmatrix} q_4 I_{3 \times 3} + [\boldsymbol{\rho} \times] \\ -\boldsymbol{\rho}^T \end{bmatrix} \boldsymbol{\omega} \equiv \frac{1}{2} \Xi(\mathbf{q}) \boldsymbol{\omega} \quad (7)$$

where $\boldsymbol{\omega}$ is the three-component angular rate vector. Successive rotations can be accomplished using quaternion multiplication. Here we adopt the convention of [1] and [7] which multiply the quaternions in the same order as the attitude matrix multiplication: $A(\mathbf{q}')A(\mathbf{q}) = A(\mathbf{q}' \otimes \mathbf{q})$, with $\mathbf{q}' \otimes \mathbf{q} = \left[\Xi(\mathbf{q}') \ ; \ \mathbf{q}' \right] \mathbf{q}$, where $\left[\Xi(\mathbf{q}') \ ; \ \mathbf{q}' \right]$ is a 4×4 augmented matrix.

Also, the inverse of the quaternion defined above is given by $\mathbf{q}^{-1} = [-\boldsymbol{\rho}^T \ q_4]^T$.

A common sensor that measures the angular rate is a rate-integrating gyro. For this sensor, a widely used model is given by [13]

$$\tilde{\boldsymbol{\omega}}(t) = \boldsymbol{\omega}(t) + \boldsymbol{\beta}(t) + \boldsymbol{\eta}_v(t) \quad (8a)$$

$$\dot{\boldsymbol{\beta}}(t) = \boldsymbol{\eta}_u(t) \quad (8b)$$

where $\tilde{\boldsymbol{\omega}}(t)$ is the continuous-time measured angular rate, $\boldsymbol{\omega}(t)$ is the true angular rate, $\boldsymbol{\beta}(t)$ is the gyro bias, and $\boldsymbol{\eta}_v(t)$ and $\boldsymbol{\eta}_u(t)$ are independent zero-mean Gaussian white-noise processes with $E\{\boldsymbol{\eta}_v(t)\boldsymbol{\eta}_v^T(\tau)\} = I_{3 \times 3}\sigma_v^2\delta(t-\tau)$ and $E\{\boldsymbol{\eta}_u(t)\boldsymbol{\eta}_u^T(\tau)\} = I_{3 \times 3}\sigma_u^2\delta(t-\tau)$, where $\delta(t-\tau)$ is the Dirac delta function.

A widely-used vector measurement model is given by

$$\tilde{\mathbf{y}}_k = \begin{bmatrix} \mathbf{b}_1 \\ \vdots \\ \mathbf{b}_m \end{bmatrix} \Big|_k + \mathbf{v}_k = \begin{bmatrix} A(\mathbf{q})\mathbf{r}_1 \\ \vdots \\ A(\mathbf{q})\mathbf{r}_m \end{bmatrix} \Big|_k + \mathbf{v}_k \quad (9)$$

where \mathbf{v}_k is a zero-mean Gaussian noise process with covariance R_k , m is the number of vector measurements, and the subscript k denotes time t_k . The vector measurement model is used to calculate the likelihood function in the weight update step of the attitude estimation particle filter.

IV. Attitude Estimation Particle Filter

Quaternions are desirable for attitude estimation because of their singularity-free property. However the norm constraint must be maintained. Straightforward implementation of the particle filter estimate, given by Eq. (5a), clearly shows that a weighted sum average of quaternions does not produce a normalized vector in general. To overcome this issue a local minimal-error representation, defined by the modified Rodrigues parameters (MRPs) [7], is used while the quaternion is maintained as the global representation. More important, the local minimal-error representation is used to calculate the matrix Σ in Eqs. (3), based on which the attitude perturbations are generated in the regularization step of the attitude estimation particle filter. In terms of the unit Euler axis \mathbf{e} and the rotation angle ϑ , the MRPs are given by $\mathbf{p} \equiv \mathbf{e} \tan(\vartheta/4)$. For small θ , $\mathbf{p} \approx \mathbf{e} \vartheta/4$. As there are always two quaternions $\pm \mathbf{q}$ that represent the same attitude, there are always two sets of MRPs, \mathbf{p} and $-\mathbf{p}/\|\mathbf{p}\|^2$, that represent the same attitude. The standard positive form of the MRPs are defined by $\mathbf{p} \equiv \text{sign}(q_4)\boldsymbol{\rho}/(1 + |q_4|)$. Note that the standard positive form has a vector that

is maintained within a unit sphere.

The state vector for the particle filter is given by $\mathbf{x} \equiv [\boldsymbol{\delta p}^T \ \boldsymbol{\beta}^T]^T$, where $\boldsymbol{\delta p}$ is the local error-MRP vector which is related to the local error-quaternion, $\boldsymbol{\delta q} \equiv [\boldsymbol{\delta \boldsymbol{\rho}}^T \ \delta q_4]^T$, through $\boldsymbol{\delta p} = f[\boldsymbol{\delta \boldsymbol{\rho}}/(1 + \delta q_4)]$, where f is chosen to be 4 so that $\boldsymbol{\delta \boldsymbol{\rho}}$ is equal to physically intuitive roll, pitch and yaw angles for small errors. The steps involved for using the local error-MRPs in a particle filter are now shown in detail.

First an initial set of particles, $\mathbf{x}_0^{(i)} \equiv [\boldsymbol{\delta p}_0^{(i)T} \ \boldsymbol{\beta}_0^{(i)T}]^T$, are drawn from the initial distribution. Because of the ambiguity of the MRP representation, the error-MRP particles are checked to make sure that they have the minimum spread (or dispersion). In many cases, this means that the error-MRP particles are within the sphere of radius f ; the ones that do not satisfy this requirement are found using the inequality $\|\boldsymbol{\delta p}_0^{(i)}\| > f$. When converted from the quaternions, the MRPs in the standard positive form automatically satisfy this inequality. States estimates at the initial time for the quaternion and gyro bias are given, denoted by $\hat{\mathbf{q}}_0^+$ and $\hat{\boldsymbol{\beta}}_0^+$, respectively. The set of initial quaternions $\mathbf{q}_0^{(i)}$ are computed by

$$\delta q_{4_0}^{(i)} = \frac{f^2 - \|\boldsymbol{\delta p}_0^{(i)}\|^2}{f^2 + \|\boldsymbol{\delta p}_0^{(i)}\|^2} \quad (10a)$$

$$\boldsymbol{\delta q}_0^{(i)} = \begin{bmatrix} (1 + \delta q_{4_0}^{(i)})\boldsymbol{\delta p}_0^{(i)} / f \\ \delta q_{4_0}^{(i)} \end{bmatrix} \quad (10b)$$

$$\mathbf{q}_0^{(i)} = \boldsymbol{\delta q}_0^{(i)} \otimes \hat{\mathbf{q}}_0^+ \quad (10c)$$

The initial weights are set to $w_0^{(i)} = 1/N$.

The next set of steps is repeated for each time propagation cycle in the PF. A discrete-time propagation is used with time interval Δt . If the inequality $\|\Delta t \boldsymbol{\omega}\| \ll 1$ is valid, which is true for most spacecraft applications, then the covariance of the discrete-time process noise derived from the models in Eqs. (7) and (8) is given by [13]

$$Q = \begin{bmatrix} (\sigma_v^2 \Delta t + \frac{1}{3} \sigma_u^2 \Delta t^3) I_{3 \times 3} & -(\frac{1}{2} \sigma_u^2 \Delta t^2) I_{3 \times 3} \\ -(\frac{1}{2} \sigma_u^2 \Delta t^2) I_{3 \times 3} & (\sigma_u^2 \Delta t) I_{3 \times 3} \end{bmatrix} \quad (11)$$

which is time invariant. The angular velocity particles are given by

$$\boldsymbol{\omega}_k^{(i)} = \tilde{\boldsymbol{\omega}}_k - \boldsymbol{\beta}_k^{(i)} + \mathbf{w}_{1_k}^{(i)} \quad (12)$$

and the bias particles are given by

$$\boldsymbol{\beta}_{k+1}^{(i)} = \boldsymbol{\beta}_k^{(i)} + \mathbf{w}_{2_k}^{(i)} \quad (13)$$

The zero-mean Gaussian samples, $\mathbf{w}_k^{(i)} = \begin{bmatrix} \mathbf{w}_{1_k}^{(i)T} & \mathbf{w}_{2_k}^{(i)T} \end{bmatrix}^T$ where $\mathbf{w}_{1_k}^{(i)}$ and $\mathbf{w}_{2_k}^{(i)}$ are 3×1 vectors, can be drawn based on a Cholesky decomposition of Q :

$$Q = S^T S = \begin{bmatrix} \sqrt{\sigma_v^2 \Delta t + \frac{1}{12} \sigma_u^2 \Delta t^3} I_{3 \times 3} & -\frac{1}{2} \sigma_u \sqrt{\Delta t^3} I_{3 \times 3} \\ 0_{3 \times 3} & \sigma_u \sqrt{\Delta t} I_{3 \times 3} \end{bmatrix} \begin{bmatrix} \sqrt{\sigma_v^2 \Delta t + \frac{1}{12} \sigma_u^2 \Delta t^3} I_{3 \times 3} & 0_{3 \times 3} \\ -\frac{1}{2} \sigma_u \sqrt{\Delta t^3} I_{3 \times 3} & \sigma_u \sqrt{\Delta t} I_{3 \times 3} \end{bmatrix}$$

The matrix S^T is used to generate $\mathbf{w}_{1_k}^{(i)}$ and $\mathbf{w}_{2_k}^{(i)}$ by weighting vectors of random samples of zero mean and unit variance. The error-quaternion for the i^{th} particle, denoted by $\boldsymbol{\delta} \mathbf{q}^{(i)} \equiv [\boldsymbol{\delta} \boldsymbol{\rho}^{(i)T} \ \delta q_4^{(i)}]^T$ is computed using

$$\delta q_{4_k}^{(i)} = \frac{f^2 - \|\boldsymbol{\delta} \mathbf{p}_k^{(i)}\|^2}{f^2 + \|\boldsymbol{\delta} \mathbf{p}_k^{(i)}\|^2} \quad (14a)$$

$$\boldsymbol{\delta} \mathbf{q}_k^{(i)} = \begin{bmatrix} (1 + \delta q_{4_k}^{(i)}) \boldsymbol{\delta} \mathbf{p}_k^{(i)} / f \\ \delta q_{4_k}^{(i)} \end{bmatrix} \quad (14b)$$

The quaternion particles at time t_k are then given by

$$\mathbf{q}_k^{(i)} = \boldsymbol{\delta} \mathbf{q}_k^{(i)} \otimes \hat{\mathbf{q}}_k^+ \quad (15)$$

where $\hat{\mathbf{q}}_k^+$ is the updated estimated quaternion at time t_k . The updated estimated quaternion is fully defined by Eq. (23). These quaternions are propagated to the next time step using

$$\mathbf{q}_{k+1}^{(i)} = \Omega(\boldsymbol{\omega}_k^{(i)}) \mathbf{q}_k^{(i)} \quad (16)$$

with

$$\Omega(\boldsymbol{\omega}_k^{(i)}) \equiv \begin{bmatrix} \cos(0.5 \|\boldsymbol{\omega}_k^{(i)}\| \Delta t) I_{3 \times 3} - [\boldsymbol{\psi}_k^{(i)} \times] & \boldsymbol{\psi}_k^{(i)} \\ -\boldsymbol{\psi}_k^{(i)T} & \cos(0.5 \|\boldsymbol{\omega}_k^{(i)}\| \Delta t) \end{bmatrix} \quad (17)$$

where $\boldsymbol{\psi}_k^{(i)} \equiv \sin(0.5 \|\boldsymbol{\omega}_k^{(i)}\| \Delta t) \boldsymbol{\omega}_k^{(i)} / \|\boldsymbol{\omega}_k^{(i)}\|$. Note that the estimated quaternion is also propagated using $\hat{\mathbf{q}}_{k+1}^- = \Omega(\hat{\boldsymbol{\omega}}_k^+) \hat{\mathbf{q}}_k^+$, where the superscript $-$ denotes a propagated quantity and $\hat{\boldsymbol{\omega}}_k^+ = \tilde{\boldsymbol{\omega}}_k - \hat{\mathbf{b}}_k^+$.

The error-quaternions at time t_{k+1} relative to $\hat{\mathbf{q}}_{k+1}^-$ are then computed using

$$\delta \mathbf{q}_{k+1}^{(i)} \equiv \begin{bmatrix} \delta \boldsymbol{\rho}_{k+1}^{(i)} \\ \delta q_{4k+1}^{(i)} \end{bmatrix} = \mathbf{q}_{k+1}^{(i)} \otimes (\hat{\mathbf{q}}_{k+1}^-)^{-1} \quad (18)$$

The propagated error-MRPs are given by

$$\delta \mathbf{p}_{k+1}^{(i)} = f \frac{\text{sign}(\delta q_{4k+1}^{(i)}) \delta \boldsymbol{\rho}_{k+1}^{(i)}}{1 + |\delta q_{4k+1}^{(i)}|} \quad (19)$$

where sign is used to maintain consistency of the error-MRPs from the previous time point.

The next step involves computing the weights in the PF. This is done by using the measurement observations. At each time step it is assumed that m vector observations are available. The likelihood function at time t_{k+1} used to update the weights is given by

$$L_{k+1}(\mathbf{x}_{k+1}^{(i)}) = p_{k+1}(\tilde{\mathbf{y}}_{k+1} | \mathbf{x}_{k+1}^{(i)}) \propto \exp \left[-\frac{1}{2} (\tilde{\mathbf{y}}_{k+1} - \mathbf{y}_{k+1}^{(i)})^T R_{k+1}^{-1} (\tilde{\mathbf{y}}_{k+1} - \mathbf{y}_{k+1}^{(i)}) \right] \quad (20)$$

where \propto stands for “proportional to” and

$$\mathbf{y}_{k+1}^{(i)} = \left[\begin{array}{c} A(\mathbf{q}^{(i)}) \mathbf{r}_1 \\ \vdots \\ A(\mathbf{q}^{(i)}) \mathbf{r}_m \end{array} \right] \Big|_{k+1} \quad (21)$$

Equation (2) is used to update the weights. Note that the inverse of R_{k+1} is required, which is singular for unit vector observations. See [14] and [15] for a discussion on this issue in attitude filtering problems and an approach to overcome it.

The next step involves computing the updated quaternion and gyro bias. Equation (5a) is used to update the state estimate $\hat{\mathbf{x}}_{k+1}^+ \equiv [\delta \hat{\mathbf{p}}_{k+1}^{+T} \hat{\mathbf{b}}_{k+1}^{+T}]^T$. The updated gyro bias is simply given by the last three elements of $\hat{\mathbf{x}}_{k+1}^+$. The updated error-quaternion is computed using

$$\delta \hat{q}_{4k+1}^+ = \frac{f^2 - \|\delta \hat{\mathbf{p}}_{k+1}^+\|^2}{f^2 + \|\delta \hat{\mathbf{p}}_{k+1}^+\|^2} \quad (22a)$$

$$\delta \hat{\mathbf{q}}_{k+1}^+ = \begin{bmatrix} (1 + \delta \hat{q}_{4k+1}^+) \delta \hat{\mathbf{p}}_{k+1}^+ / f \\ \delta \hat{q}_{4k+1}^+ \end{bmatrix} \quad (22b)$$

and the updated quaternion is given by

$$\hat{\mathbf{q}}_{k+1}^+ = \delta \hat{\mathbf{q}}_{k+1}^+ \otimes \hat{\mathbf{q}}_{k+1}^- \quad (23)$$

It is important to note that quaternion normalization is maintained throughout the entire process without any further steps to do so.

A complete cycle of the attitude estimation PF including resampling and regularization is summarized as follows:

- Prediction

1. Propagate $\boldsymbol{\beta}_k^{(i)} \rightarrow \boldsymbol{\beta}_{k+1}^{(i)}$ using Eq. (13).
2. Compute $\boldsymbol{\omega}_k^{(i)}$ using Eq. (12) and compute $\hat{\boldsymbol{\omega}}_k^+ = \tilde{\boldsymbol{\omega}}_k - \hat{\boldsymbol{\beta}}_k^+$, where $\hat{\boldsymbol{\beta}}_k^+$ is obtained from the weighted sum particles of the update stage.
3. Propagate $\mathbf{q}_k^{(i)} \rightarrow \mathbf{q}_{k+1}^{(i)}$ through the quaternion kinematics using Eq. (16), and also propagate $\hat{\mathbf{q}}_k^+ \rightarrow \hat{\mathbf{q}}_{k+1}^-$ using $\hat{\boldsymbol{\omega}}_k^+$.

- Update

1. Compute the likelihood functions $L_{k+1}(\mathbf{x}_{k+1}^{(i)})$ using Eq. (20).
2. Update the particle weights $w_{k+1}^{(i)}$ with the likelihood functions using Eq. (2).
3. Compute $\boldsymbol{\delta}\mathbf{q}_{k+1}^{(i)}$ using Eq. (18).
4. Convert $\boldsymbol{\delta}\mathbf{q}_{k+1}^{(i)} \rightarrow \boldsymbol{\delta}\mathbf{p}_{k+1}^{(i)}$ using Eq. (19).
5. Compute the mean MRPs $\boldsymbol{\delta}\hat{\mathbf{p}}_{k+1}^+$ and the mean gyro bias $\hat{\boldsymbol{\beta}}_{k+1}^+$ using Eq. (5a).
6. Compute $\hat{\mathbf{q}}_{k+1}^+$ using Eq. (23).
7. Compute the matrix Σ_{k+1} using Eq. (3).
8. Resample to obtain N copies of $\boldsymbol{\delta}\mathbf{p}_{k+1}^{(i)}$ and $\boldsymbol{\beta}_{k+1}^{(i)}$ and set $w_{k+1}^{(i)}$ to $1/N$.
9. Perturb $\boldsymbol{\delta}\mathbf{p}_{k+1}^{(i)}$ and $\boldsymbol{\beta}_{k+1}^{(i)}$ by adding zero-mean Gaussian noise of covariance $h^2\Sigma_{k+1}$ to them.
10. Compute $\mathbf{q}_{k+1}^{(i)}$ by “adding” the perturbed $\boldsymbol{\delta}\mathbf{p}_{k+1}^{(i)}$ to $\hat{\mathbf{q}}_{k+1}^-$.

The above PF does not work well unless the number N of particles is large enough. With large initial errors, small process noise (gyro measurement noise), and a narrow likelihood function (the effective measurement noise of attitude sensors onboard most spacecraft is below one degree with that of a star tracker in the order of arcseconds), no initial attitude particles are likely to be in the significant regions of the likelihood functions. In most cases, only one or very few particles have large weights initially. The resampling step that follows discards most particles, so the PF immediately loses particle diversity, and the particle cloud collapses into those few particles with large weights.

To overcome this problem, the principle of progressive correction [5] splits the original likelihood function into n likelihood functions: $L_{k+1}(\mathbf{x}_{k+1}) = \prod_{j=1}^n L_{k+1}^{1/\lambda_{k+1}^{(j)}}(\mathbf{x}_{k+1})$, where

$\lambda_{k+1}^{(j)} > 1$ and $\sum_{j=1}^n 1/\lambda_{k+1}^{(j)} = 1$. Given the measurement vector $\tilde{\mathbf{y}}_{k+1}$, the particles are updated with n identical fictitious measurements $\tilde{\mathbf{y}}_{k+1}$ at t_{k+1} , for which the likelihood functions are $L_{k+1}^{1/\lambda_{k+1}^{(j)}}(\mathbf{x}_{k+1})$. The updates are implemented by the repeated use of the aforementioned nine steps. A new quaternion reference $\hat{\mathbf{q}}_{k+1}^-$ is needed for each update, and therefore $\hat{\mathbf{q}}_{k+1}^-$ is set to $\hat{\mathbf{q}}_{k+1}^+$ at the end of an update, following Step 9. Note that Step 9 is the only step at the update stage that provides new particles, some of which are likely to agree with the measurement better than the particles directly propagated through the dynamical model. This amounts to a local random search of the state space for better particles.

For the likelihood function given by Eq. (20), $L_{k+1}^{1/\lambda_{k+1}^{(j)}}(\mathbf{x}_{k+1})$ is equal to $L_{k+1}(\mathbf{x}_{k+1})$ where R_{k+1} is replaced by $\lambda_{k+1}^{(j)} R_{k+1}$. Greater-than-one $\lambda_{k+1}^{(j)}$ increases the spread of the likelihood function and reduces the variance of the corresponding particle weights, which reduces the number of particles eliminated by the resampling step. The idea of using wider likelihood functions to retain particle diversity has been employed in [16,10] as well. A decreasing sequence in general, they are computed from the particles as

$$\lambda_{k+1}^{(j)} = \max \left(1, \frac{\max_i L_{k+1}(\mathbf{x}_{k+1}^{(i)})}{\log(\delta_{\max})} \right) \quad (24)$$

where δ_{\max} is a tuning parameter. Small δ_{\max} results in large $\lambda_{k+1}^{(j)}$. See [5] for useful relations about δ_{\max} and examples.

Modification of the progressive correction method is made when it is applied to spacecraft attitude estimation with extremely poor initial guesses and single vector observations. It is observed that using large $\lambda_{k+1}^{(j)}$ in the initialization phase is essential to the convergence of the PF from extremely large initial errors. Measures are taken to ensure that $\lambda_{k+1}^{(i)}$ does not go too small while the attitude errors are large. The number of progressive corrections at each measurement time is limited to two because a large number of progressive corrections causes significant biased errors [5] and more importantly may eliminate too many particles too quickly. After $\lambda_{k+1}^{(1)}$ is computed using Eq. (24), it is increased to the nearest member of a predetermined set. For example, if $\lambda_{k+1}^{(1)}$ is between 10 and 100, it is replaced by 100; if $\lambda_{k+1}^{(1)}$ is between 100 and 1000, it is replaced by 1000; and so on. In addition, $\lambda_{k+1}^{(2)}$ is chosen as the larger of $0.5\lambda_{k+1}^{(1)}$ and the value computed using Eq. (24). Note that $\lambda_{k+1}^{(j)}$ computed this way does not necessarily satisfy $\sum_{j=1}^n 1/\lambda_{k+1}^{(j)} = 1$. When that is the case, i.e., $\sum_{j=1}^n 1/\lambda_{k+1}^{(j)} < 1$, the information contained in the measurements is not made full use of in the Bayesian sense.

V. Simulation Example

In this section a simulation is shown that compares the convergence performance of the PF to the UKF and EKF in the presence of large initialization errors. The values of the main parameters of the PF are: the number of particles $N = 2000$, the perturbation level $h = 0.1$, the number of progressive corrections $n = 2$, and the progressive correction parameter $\delta_{\max} = e^6 \approx 403$. The PF is implemented in MATLAB.

The simulation is taken directly from [2], which involves an Earth-pointing spacecraft in a near-circular 90 min (350 km) orbit with an inclination of 35° . The nominal Earth-pointing mission mode requires a rotation once per orbit about the spacecraft's y -axis. The simulation shown here assumes only TAM and gyro measurements. The magnetic field reference is modeled using a 10th-order International Geomagnetic Reference Field model [17]. TAM sensor noise is modeled by a zero-mean Gaussian white-noise process with a standard deviation of 30 nT. The gyro measurements are simulated using $\sigma_u = 3.1623 \times 10^{-4} \mu\text{rad}/\text{sec}^{3/2}$ and $\sigma_v = 0.31623 \mu\text{rad}/\text{sec}^{1/2}$, and an initial bias of 0.1 deg/hr on each axis.

Attitude errors of -50° , 50° and 160° for each axis, respectively, are added into the initial-condition attitude estimate. The initial attitude covariance is set to $(50 \text{ deg})^2$ for each attitude component. The initial x - and z -axes estimates for the gyro biases are set to zero, however the initial y -axis bias estimate is 20 deg/hr. The initial bias covariance is set to $(20 \text{ deg/hr})^2$ for each axis. The initial particles are drawn using a Gaussian distribution with the aforementioned covariance matrices, which ensures that each filter is initialized in a consistent manner.

A plot of the norm of the attitude errors for this simulation case is shown in Figure 1. The EKF does not converge for this case since the first-order approximation cannot adequately capture the large initial condition errors. The UKF does have better convergence properties than the EKF for this case, however the PF provides the best convergence performance. Both the EKF and the UKF are more sensitive to the initial conditions than the PF. The steady-state accuracy is consistent with that in [2]. The accuracy is high because the only error in the measurement model is additive, zero-mean, Gaussian white noise in the magnetometer frame representation of the magnetic field vector only. In more realistic scenarios, the accuracy of a magnetometer-based attitude determination system is generally about two degrees. With careful calibration and design, sub-arc-minute accuracy can be achieved [18]. Because the PF makes extensive use of pseudo-random numbers, its estimates vary from run to run even if the same measurements are processed. The performance of the PF is checked by running the filter 100 times. It always converges and the statistics of the estimation results in the fifty runs are almost identical.

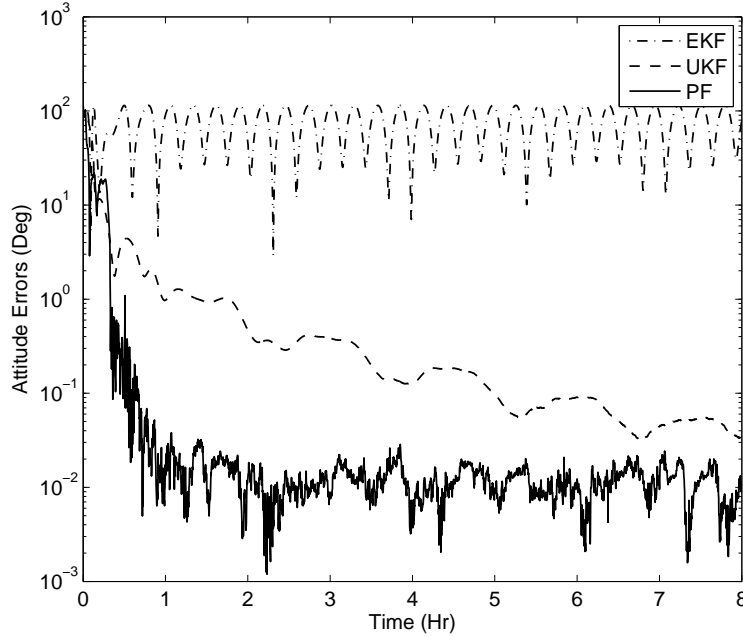


Figure 1. Norm of Attitude Errors

VI. Conclusions

In this paper a new formulation for attitude estimation using a particle filter was shown. The approach developed in this paper used an unconstrained three-dimensional vector for the local-error representation while using the quaternion for the global representation. In this approach the unconstrained local-error particles can be used directly in the particle filter. Also, the conversion from the local-error representation to the global representation requires less computations than implementing a strategy that explicitly maintains quaternion normalization. Although the particle filter shown in this paper is based on the bootstrap filter, the local/global representation can be still applied to any particle filter formulation. Simulation results indicated that the performance of the new filter based on the idea of progressive correction far exceeds the standard extended Kalman and unscented Kalman filter for large initialization errors.

References

- ¹Lefferts, E. J., Markley, F. L., and Shuster, M. D., “Kalman Filtering for Spacecraft Attitude Estimation,” *Journal of Guidance, Control, and Dynamics*, Vol. 5, No. 5, Sept.-Oct. 1982, pp. 417–429.
- ²Crassidis, J. L. and Markley, F. L., “Unscented Filtering for Spacecraft Attitude Estimation,” *Journal of Guidance, Control and Dynamics*, Vol. 26, No. 4, July-Aug. 2003, pp. 536–542.
- ³Crassidis, J. L., Markley, F. L., and Cheng, Y., “A Survey of Nonlinear Attitude Estimation Methods,”

Journal of Guidance, Control and Dynamics, Vol. 30, No. 1, Jan.-Feb. 2007, pp. 12–28.

⁴Arulampalam, M. S., Maskell, S., Gordon, N., and Clapp, T., “A Tutorial on Particle Filters for Online Nonlinear/Non-Gaussian Bayesian Tracking,” *IEEE Transactions on Signal Processing*, Vol. 50, No. 2, Feb. 2002, pp. 174–185.

⁵Musso, C., Oudjane, N., and Gland, F. L., “Improving Regularized Particle Filters,” *Sequential Monte Carlo Methods in Practice*, edited by A. Doucet, N. de Freitas, and N. Gordon, chap. 12, Springer-Verlag, New York, NY, 2001.

⁶Oshman, Y. and Carmi, A., “Attitude Estimation from Vector Observations Using a Genetic-Algorithm-Embedded Quaternion Particle Filter,” *Journal of Guidance, Control and Dynamics*, Vol. 29, No. 4, July-Aug. 2006, pp. 879–891.

⁷Shuster, M. D., “A Survey of Attitude Representations,” *Journal of the Astronautical Sciences*, Vol. 41, No. 4, Oct.-Dec. 1993, pp. 439–517.

⁸Markley, F. L., Cheng, Y., Crassidis, J. L., and Oshman, Y., “Averaging Quaternions,” *Journal of Guidance, Control and Dynamics*, Vol. 30, No. 4, July-Aug. 2007, pp. 1193–1196.

⁹Psiaki, M. L., “Estimation Using Quaternion Probability Densities on the Unit Hypersphere,” *Journal of the Astronautical Sciences*, Vol. 54, No. 3-4, July-Dec. 2006, pp. 415–431.

¹⁰Carmi, A. and Oshman, Y., “Fast Particle Filtering for Attitude and Angular-Rate Estimation from Vector Observations,” *Journal of Guidance, Control, and Dynamics*, Vol. 21, No. 1, Jan.-Feb. 2009, pp. 70–78.

¹¹Gordon, N. J., Salmond, D. J., and Smith, A. F. M., “Novel Approach to Nonlinear/Non-Gaussian Bayesian State Estimation,” *Radar and Signal Processing, IEE Proceedings F*, Vol. 140, No. 2, April 1993, pp. 107–113.

¹²Doucet, A., de Freitas, N., and Gordon, N., “An Introduction to Sequential Monte Carlo Methods,” *Sequential Monte Carlo Methods in Practice*, edited by A. Doucet, N. de Freitas, and N. Gordon, chap. 1, Springer-Verlag, New York, NY, 2001.

¹³Farrenkopf, R. L., “Analytic Steady-State Accuracy Solutions for Two Common Spacecraft Attitude Estimators,” *Journal of Guidance and Control*, Vol. 1, No. 4, July-Aug. 1978, pp. 282–284.

¹⁴Shuster, M. D., “Kalman Filtering of Spacecraft Attitude and the QUEST Model,” *Journal of the Astronautical Sciences*, Vol. 38, No. 3, July-Sept. 1990, pp. 377–393.

¹⁵Cheng, Y., Crassidis, J. L., and Markley, F. L., “Attitude Estimation for Large Field-of-View Sensors,” *The Journal of the Astronautical Sciences*, Vol. 54, No. 3/4, July-Dec. 2006, pp. 433–448.

¹⁶Cheng, Y. and Crassidis, J. L., “Particle Filtering for Sequential Spacecraft Attitude Estimation,” *Proceedings of AIAA Guidance, Navigation, and Control Conference*, Providence, Rhode Island, August 2004.

¹⁷Langel, R. A., “International Geomagnetic Reference Field: The Sixth Generation,” *Journal of Geomagnetism and Geoelectricity*, Vol. 44, No. 9, 1992, pp. 679–707.

¹⁸Hashmall, J. and Sedlak, J., “The Use of Magnetometers for Accurate Attitude Determination,” *Proceedings of the 12th International Symposium on Space Flight Dynamics*, Darmstadt, Germany, July 1997, pp. 179–184.